

# Static And Buckling Analysis of Fuselage Panel under Varied Flight Condition's

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**Abstract:-** Designers need to guarantee the security of structure all through administration life for which structure is being designed. To guarantee wellbeing of the structure, designer ought to first see how a structure would fall flat. There are two sorts of disappointments one is material disappointment other is basic disappointment. Buckling drops into the classification of auxiliary disappointment approach. Fuselage is part, which houses the travellers and load on account of a common transport air ship. For the most part it is a barrel with orthogonally hardened developed development. The flying machine will be in harmony at any moment of time amid flying. Fuselage will encounter fundamentally the latency and pressurization loads. This anticipates incorporates a linear static and linear buckling investigation of the front fuselage assembly. Contingent upon mass dissemination of the fuselage structure the dormancy strengths will change along with length of fuselage. Inactivity power dissemination creates fuselage to twist descending around wing hub. This bending of fuselage will make strain and pressure in upper and lower fuselage hardened boards individually. Current study incorporates, the topic of pressure buckling of boards in base part of fuselage. A linear static investigation will be done on section of front fuselage assembly with circulated air weight following up on it. Boards with greatest pressure burden will recognized as basic boards for buckling investigation. Pivotal pressure weight following up on every board be separated from the static investigation. Established methodology will be taken after to figure the basic buckling weight on every board. These counts will be verified by board buckling investigation through finite element met

**Keywords-** fuselage panel, Buckling Analysis, Static analysis, Mach number.

## 1. INTRODUCTION

A plane is a mind-boggling structure, yet a flying machine made by the extremely effective man. Aircraft are generally one or more particular capacities and ought to be designed to guarantee it can perform these capacities securely. Any title disappointment of any of these parts can prompt a calamitous debacle bringing about extraordinary demolition of life and property. In the design of a plane, it's about finding the ideal proportion of vehicle weight and payload. It must be solid and adequate to bolster the outstanding circumstances in which it needs to work. Sturdiness is a critical element. Likewise, if a section falls flat, it not as a matter of course results in disappointment of the whole aircraft. It is still feasible for the aircraft to slide over to a protected landing put just if the streamlined shape is held auxiliary honesty is accomplished.

The essential elements of the structure of an aircraft are to transmit and withstand the connected burdens; to give a streamlined shape and to ensure passengers, payload frameworks, and so on., of the ecological conditions experienced in flight. These prerequisites, in most aircraft,

offer ascent to thin film structures, wherein the external surface of the skin or shell is generally bolstered by individuals from longitudinal fortification and transverse ribs in order to oppose the bending and compression loads without disfiguring torsion. Such structures are known as Semi monologue, while dainty shells that depend completely on their skins for their capacity to withstand burdens are known as monologue.

### *Aircraft Component a. Fuselage*



**Figure 1 Fuselage**

Fuselage depends on the French fuseler mouth, which signifies "think". The principle body structure is the fuselage to which every other part are joined. The fuselage containing cockpit or flight, traveler compartment, payload and wings create greater part of lift, the body likewise delivers some lift.

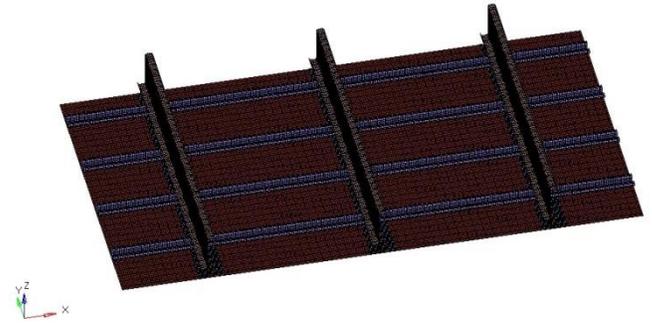
**2.LITERATURE SURVEY**

Finite element buckling analysis of hardened plates with fileted intersections was examined and researched by Patrick E. Fenner, Andrew Watson[1]. They concentrated on the impact of changing the cross area of a solidified board and the impact on its execution on buckling load. The correlation of the line intersection geometry between a fileted and non-fileted intersection with a scope of filet radii were dissected and exhibited. Diagnostic results and numerical results were obtained utilizing VINOCOPT and MSC NASTRAN. The study demonstrates that the hardened board with a filet sweep of 5 mm has an underlying buckling stress of 40.18 MPa contrasted with the square intersection consequence of 31.57 MPa.

A study on Flexible/plastic buckling of isotropic slim plates exposed to constant and linearly changing in-plane stacking utilizing incremental and disfigurement speculations was concentrated on by M.Kadkhodayan et al[2]. In their study, the harmony and security conditions for flimsy rectangular plate in plastic mode under different loadings were gotten. The outcomes were contrasted with beforehand distributed information with check the built up methodology and strategies. The angle proportion has significant impact on the buckling coefficient in IT particularly for biaxial compression/strain stacking.

EirikByklum et al.,[3] exhibited the paper on semi expository model for worldwide buckling and post buckling analysis of hardened boards. Computational model for worldwide buckling and post buckling analysis of solidified boards was inferred. Biaxial in-plane compression or strain, shear, and parallel weight burdens were considered. Diversions are accepted as trigonometric capacity arrangement, and the standard of stationary potential vitality is utilized for inferring, the balance conditions. The stress values at basic focuses at every augmentation helped with comprehension a definitive quality of boards. Utilizing the von Mises yield basis, onset of yielding taken as breakdown weight for design purposes. This is traditionalist, and sound, design method, since yielding will give undesirable perpetual distortions in the structure.

**3. FINITE ELEMENT MODELING**



*Figure 2 - FE Model of the fuselage panel*

**Material Properties**

The materials used for the analysis are Al7075 and Al2024-T351.

**Aluminium alloy Al7075-T6**

**Table 1: Mechanical properties of 7075-T6 Aluminium alloy**

Young's modulus	71700 N/mm <sup>2</sup>
Poisson's ratio	0.33
Density	2.81 X 10 <sup>-6</sup> kg/mm <sup>3</sup>
Tensile yield strength	503 N/mm <sup>2</sup>
Tensile ultimate strength	572 N/mm <sup>2</sup>

**Aluminium alloy Al2024-T351**

**Table 2: Material Properties in Al 2024-T351**

Properties	Material
Young's modulus	73100 N/mm <sup>2</sup>
Poisson's ratio	0.3
Density	2.78 X 10 <sup>-6</sup> kg/mm <sup>3</sup>
Tensile yield strength	345 N/mm <sup>2</sup>
Tensile ultimate strength	483 N/mm <sup>2</sup>

**CALCULATIONS**

Air density at the height of 3000 m = 0.905 kg/m<sup>3</sup>

**Table 3: Panel details**

Mach Number	M	0.8	
Fuselage radius	r	975	mm

Skin thickness	t	1.8	mm
Length of panel	L	1543.826	mm
Breadth of panel	B	1295	mm

The Mach number considered for the aircraft is 0.8. At an altitude of 3000 m, the speed of sound reduces to 328.400 m/s. Hence,

$$\begin{aligned} \text{Speed of the aircraft} &= \text{Mach no} * \text{speed of sound} \\ &= 0.8 * 328.4 \\ &= 262.720 \text{ m/s} \end{aligned}$$

$$\text{Pressure } P_d = \frac{1}{2} \rho v^2 \text{ (Pa)}$$

Where,

$\rho$  = Density of air (kg/m<sup>3</sup>)

v = Velocity of the aircraft (m/s)

Since the objective of this work is to consider different loading conditions, the pressure obtained from the above equation has increased using design multiplier to determine the maximum design load that the model can withstand.

**Table Error! No text of specified style in document. : Design loads considered**

Air pressure (M Pa)			
1	3	5	7
0.0312	0.0937	0.1562	0.2186

Therefore,

$$\begin{aligned} P_d &= 0.5 * 0.905 * (262.720)^2 \\ &= 31232.554 \text{ Pa} = 0.0312 \text{ MPa} \end{aligned}$$

$P_d$  is the total pressure applied on the skin of the centre fuselage for the analysis.

These pressure values are used to calculate the hoop stress or circumferential stress values. The formula for hoop stress is given as

$$\sigma_c = \frac{Pr}{t}$$

Where,

P = pressure or load applied

r = radius of the panel

t = thickness of the panel

The values are given in table 4-8.

**Table 5: Circumferential stress values**

Circumferential/Hoop Stress			
1	3	5	7
16.9176	50.7529	84.5882	118.4234

The hoop stress values obtained are used to calculate the total load applied on the panel.

We know that,

$$\begin{aligned} \text{Load} &= \text{stress} * \text{area of cross section} \\ &= 16.9176 * 1543.826 * 1.8 \\ &= 47012.189 \text{ N} \end{aligned}$$

**Table 6 : Load calculation for different g loads**

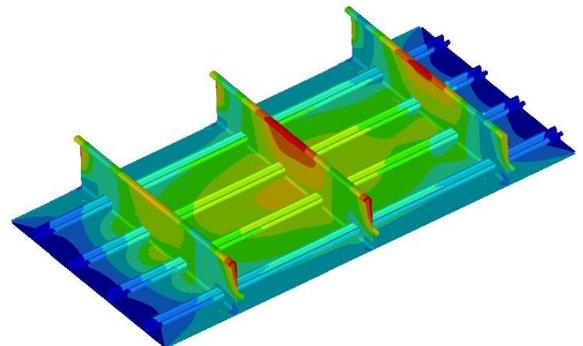
Force			
1	3	5	7
47012.1888	141036.5664	235060.9441	329085.3217

## 4.RESULTS AND DISCUSSION

The analysis was run for the above mentioned FE Model with the loads and boundary conditions attached to it. The following figures give the results obtained from both the static analysis (Displacement and Stresses) and buckling analysis (Buckling mode).

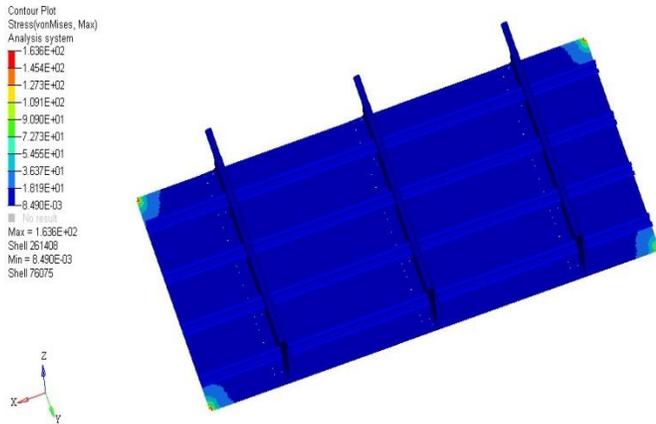
### 4.1 LINEAR STATIC ANALYSIS

#### 4.1.1 Design load – 1g



**Figure 3-1: Displacement plot for fuselage panel at 1g load**

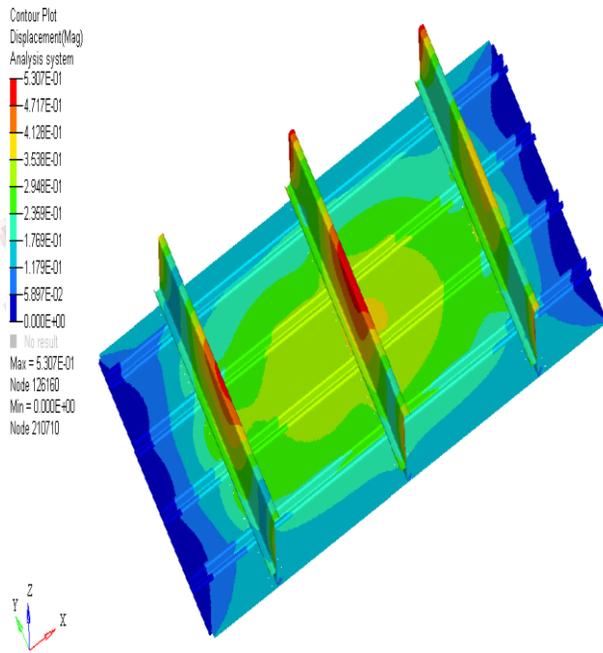
The maximum displacement is seen on the stiffeners as they are not considered to be constrained. The maximum displacement value is 0.1769 mm.



**Figure 3-2: Stress plot for fuselage panel at 1g load**

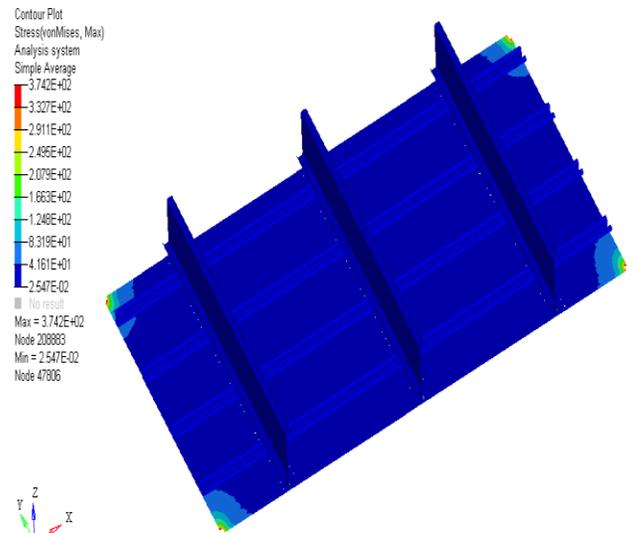
The maximum stress is located near the edges of the panel as the load was applied in the circumferential direction. The maximum stress is seen to be 163.6 MPa is less the yield strength of the material used for the fuselage panel.

**4.1.2 Design load – 3g**



**Figure 4-1: Displacement plot for fuselage panel at 3g load**

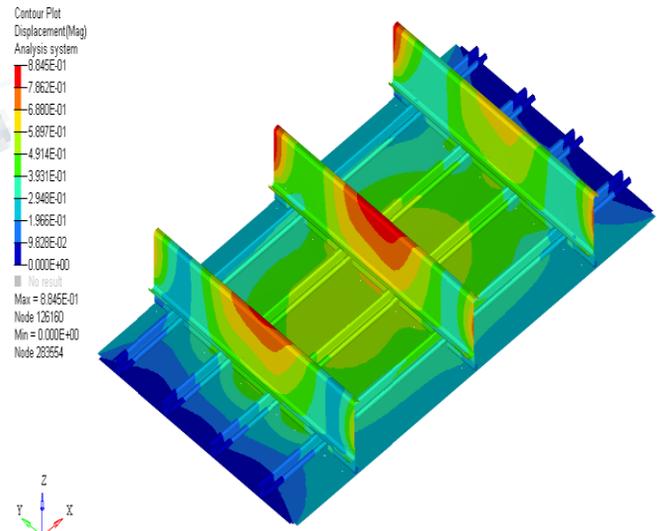
The maximum displacement is seen on the stiffeners as they are not considered to be constrained. The maximum displacement value is 0.5307 mm.



**Figure 4.2: Stress plot for fuselage panel at 3g load**

The maximum stress is located near the edges of the panel as the load was applied in the circumferential direction. The maximum stress is seen to be 374.2 MPa is less the yield strength of the material used for the fuselage panel.

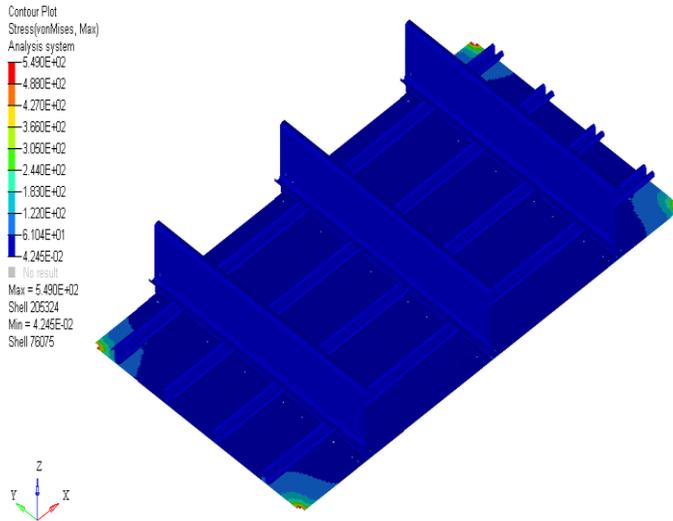
**4.1.3 Design load – 5g**



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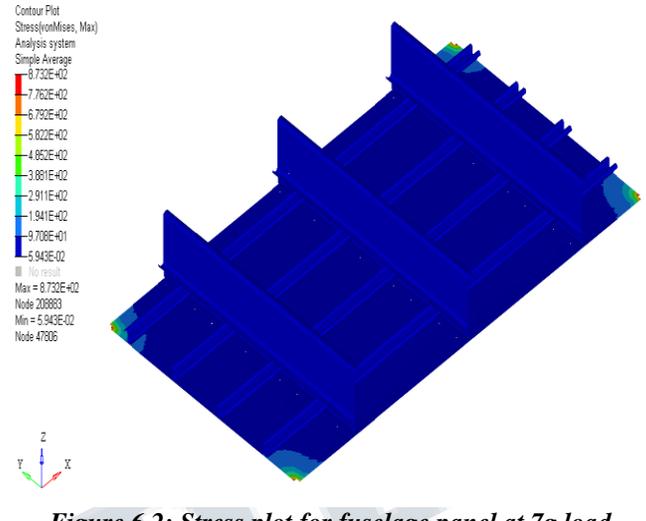
Displacement plot for fuselage panel at 5g load

The maximum displacement is seen on the stiffeners as they are not considered to be constrained. The maximum displacement value is 0.8845 mm.



**Figure 6-1: Displacement plot for fuselage panel at 7g load**

The maximum displacement is seen on the stiffeners as they are not considered to be constrained. The maximum displacement value is 1.238 mm.



**Figure 6.2: Stress plot for fuselage panel at 7g load**

The maximum stress is located near the edges of the panel as the load was applied in the circumferential direction. The maximum stress is seen to be 873.2 MPa is more the yield strength of the material used for the fuselage panel.

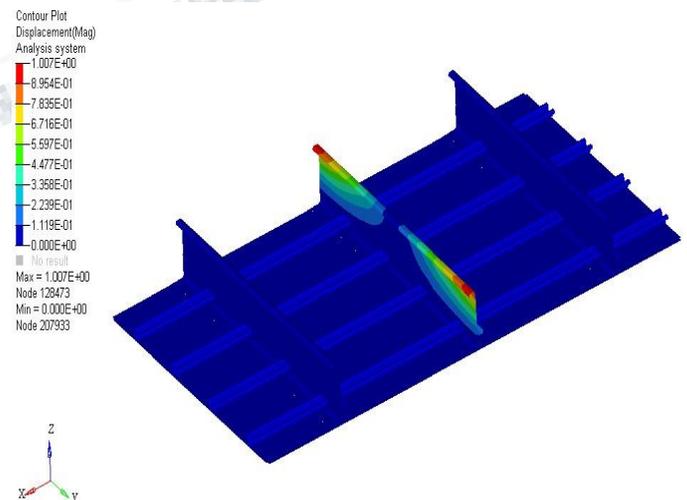
**Figure Error! No text of specified style in document.-2: Stress plot for fuselage panel at 5g load**

The maximum stress is located near the edges of the panel as the load was applied in the circumferential direction. The maximum stress is seen to be 549 MPa which is close to the yield strength of the material used for the fuselage panel.

## 4.2 BUCKLING ANALYSIS RESULTS

### 4.2.1 Design load – 1g

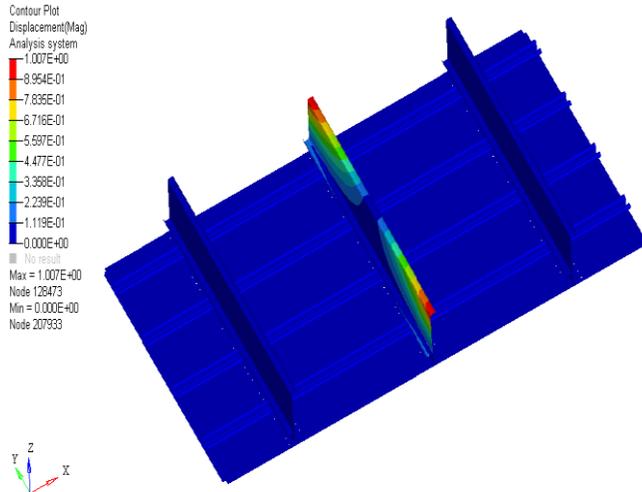
### 4.1.4 Design load – 7g



**Figure 7.1: Buckling mode plot for fuselage panel at 1g load**

The buckling factor of the panel under this load is seen to be 27.401. This value is higher than 1 which is considered as a standard for measuring the buckling of any model.

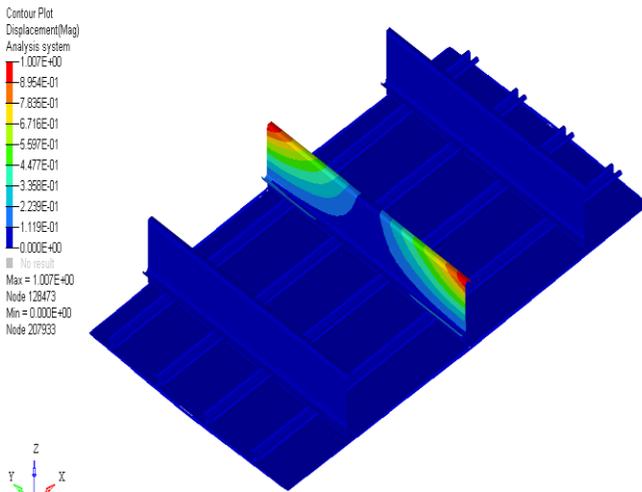
**4.2.2 Design load – 3g**



**Figure 7.2: Buckling mode plot for fuselage panel at 3g load**

The buckling factor of the panel under this load is seen to be 9.133. This value is higher than 1 which is considered as a standard for measuring the buckling of any model.

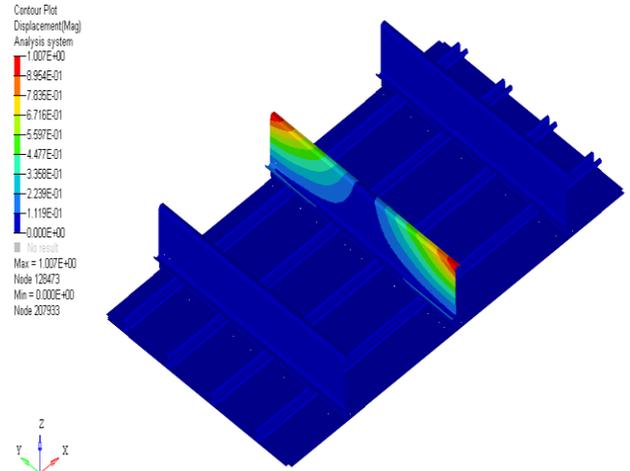
**4.2.3 Design load – 5g**



**Figure 8.1: Buckling mode plot for fuselage panel at 5g load**

The buckling factor of the panel under this load is seen to be 5.481. This value is higher than 1 which is considered as a standard for measuring the buckling of any model.

**4.2.4 Design load – 7g**



**Figure 8.2: Buckling mode plot for fuselage panel at 7g load**

The buckling factor of the panel under this load is seen to be 3.915. This value is higher than 1 which is considered as a standard for measuring the buckling of any model.

**5. CONCLUSION**

In this work, a fuselage panel was considered for analysis. The fuselage panel considered was modelled, discretized and analysed to determine its static and buckling strength due to the varying loads. It can be concluded, based on the results presented in this work, that

1. The displacement occurring in the fuselage panel for all the loading conditions is minimum and does not have considerable effect on the panel integrity.
2. The linear static analysis of the panel under the considered loads show that the panel can withstand a maximum design loading of 5g under the given conditions.
3. At 5g loading the stress level in the panel crosses the yield strength of the material considered and a small modification to the panel can reduce the stress value to be within the yield strength of material.
4. buckling analysis of the panel under the given conditions revealed that the panel can withstand well over 7g of loading even if the stress value at that load exceeds the yield point of the material.

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